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## Supporting Online Material for

### Negative Refraction at Visible Frequencies

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#### This file includes:

SOM Text

Figs. S1 and S2

References

**Correction (27 April 2007):** The following typos have been corrected:

- 1) Section 1, first paragraph, line 3:  $\hat{\mathbf{k}} = \mathbf{k} / k$  replaces  $\hat{\mathbf{k}} = |\mathbf{k}| / k$ .
- 2) Section 2, line 13:  $n_2 = \lambda_0 / P$  replaces  $n_2 = 2\lambda_0 / P$ .
- 3) Fig. S1, caption:  $n_2 = \lambda_0 / P$  replaces  $n_2 = 2\lambda_0 / P$ .

## 1. Negative index and negative refraction

Consider an electromagnetic mode propagating with wavevector  $\mathbf{k}$  in an isotropic medium. The phase and group velocity of this mode are collinear and given by, respectively,  $\mathbf{v}_p = (\omega/k)\hat{\mathbf{k}}$  and  $\mathbf{v}_g = (d\omega/dk)\hat{\mathbf{k}}$ , where  $k = |\mathbf{k}|$ , and  $\hat{\mathbf{k}} = \mathbf{k}/k$ . The phase velocity characterizes the speed and direction of propagation of the phase fronts, whereas the group velocity determines the direction of power flow  $\mathbf{S} = \mathbf{E} \times \mathbf{H} = W \mathbf{v}_g$ , where  $\mathbf{S}$  is the Poynting vector and  $W$  is the energy density of the electromagnetic field.

When  $d\omega/dk > 0$ ,  $\mathbf{v}_p$  and  $\mathbf{v}_g$  are parallel and the standard forward-wave condition  $\mathbf{v}_p \cdot \mathbf{v}_g > 0$  is obtained.  $\mathbf{k}$  and  $\mathbf{S}$  are parallel under such a condition and power propagates in the same direction as the phase-fronts. When  $d\omega/dk < 0$ ,  $\mathbf{v}_p$  and  $\mathbf{v}_g$  are anti-parallel and the anomalous backward-wave condition  $\mathbf{v}_p \cdot \mathbf{v}_g < 0$  is obtained.  $\mathbf{k}$  and  $\mathbf{S}$  are anti-parallel and power propagates in a direction opposite to that of the phase-fronts.

When a plane wave traveling in medium 1, characterized by phase and group velocities  $\mathbf{v}_p^1$  and  $\mathbf{v}_g^1$ , is incident at an angle  $\varphi_1$  upon a boundary with medium 2, characterized by phase and group velocities  $\mathbf{v}_p^2$  and  $\mathbf{v}_g^2$ , the resulting refraction angle of the transmitted beam,  $\varphi_2$ , is dictated by conservation of the parallel component of  $\mathbf{k}$  across the boundary as well as conservation of energy (see ref. S1):

$$\frac{\sin(\varphi_2)}{\sin(\varphi_1)} = \frac{\text{sign}(\mathbf{v}_p^1 \cdot \mathbf{v}_g^1) c / |\mathbf{v}_p^1|}{\text{sign}(\mathbf{v}_p^2 \cdot \mathbf{v}_g^2) c / |\mathbf{v}_p^2|} \equiv \frac{n_1}{n_2}. \quad (\text{S1})$$

By analogy with the classical form of the Snell-Descartes law of refraction  $\sin(\varphi_2)/\sin(\varphi_1) = n_1/n_2$ , an effective refractive index for each medium can be identified based on Eq. S1:

$$n_{1,2} = \text{sign}(\mathbf{v}_p^{1,2} \cdot \mathbf{v}_g^{1,2}) c / |\mathbf{v}_p^{1,2}|. \quad (\text{S2})$$

If  $\mathbf{v}_p^i \cdot \mathbf{v}_g^i < 0$ , medium  $i$  acts as if it had a negative index of refraction. When light exits such a medium into a second medium characterized by a positive index of refraction, it will be refracted, according to Eq. (S1), to the same side of the normal, i.e. to a negative angle.

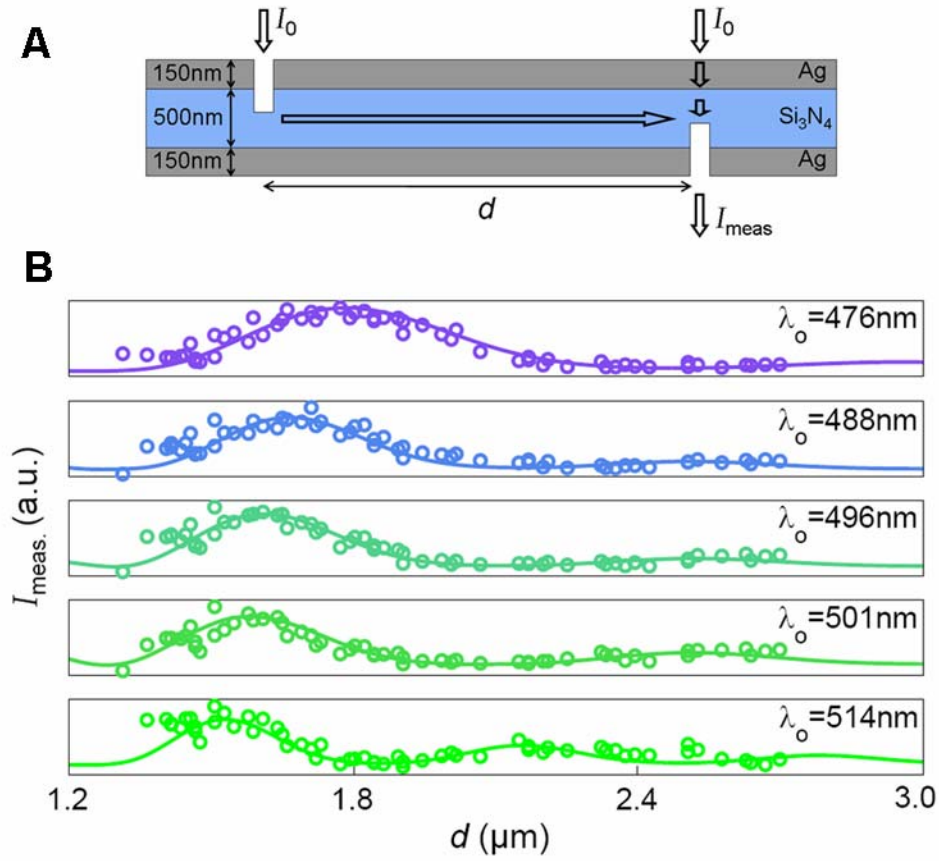
## 2. Derivation of mode index of thick Ag/Si<sub>3</sub>N<sub>4</sub>/Ag waveguide

To derive the actual value of the mode index of the thin Ag/Si<sub>3</sub>N<sub>4</sub>/Au waveguide,  $n_1$ , the mode index in the surrounding Ag/Si<sub>3</sub>N<sub>4</sub>/Ag waveguide,  $n_2$ , must be known. To circumvent the difficulty of estimating  $n_2$  theoretically, given the predicted multimodal dispersion properties (Fig. 1A), we measure  $n_2$  directly using an interferometric technique. To this end, Ag/Si<sub>3</sub>N<sub>4</sub>/Ag waveguides with 500-nm-thick dielectric cores were fabricated with semi-transparent Ag cladding layers of 150nm on each side; no additional Al cladding layer was added. The separation between input and output slit was varied from  $d = 1 \mu\text{m}$  to  $3 \mu\text{m}$  in 25-nm increments. Each device was illuminated at normal incidence over its entire area and the intensity emitted from the output slit was monitored (Fig. S1 A). Due to interference at the output-slit, between light transmitted along the waveguide and light transmitted directly through the top Ag cladding layer, a periodic modulation in the emitted intensity is obtained as a function of  $d$  (Fig. S1 B). At a given wavelength  $\lambda_0$ , the effective mode index of the waveguide is given by  $n_2 = \lambda_0 / P$ , where  $P$  is the period of the modulation.

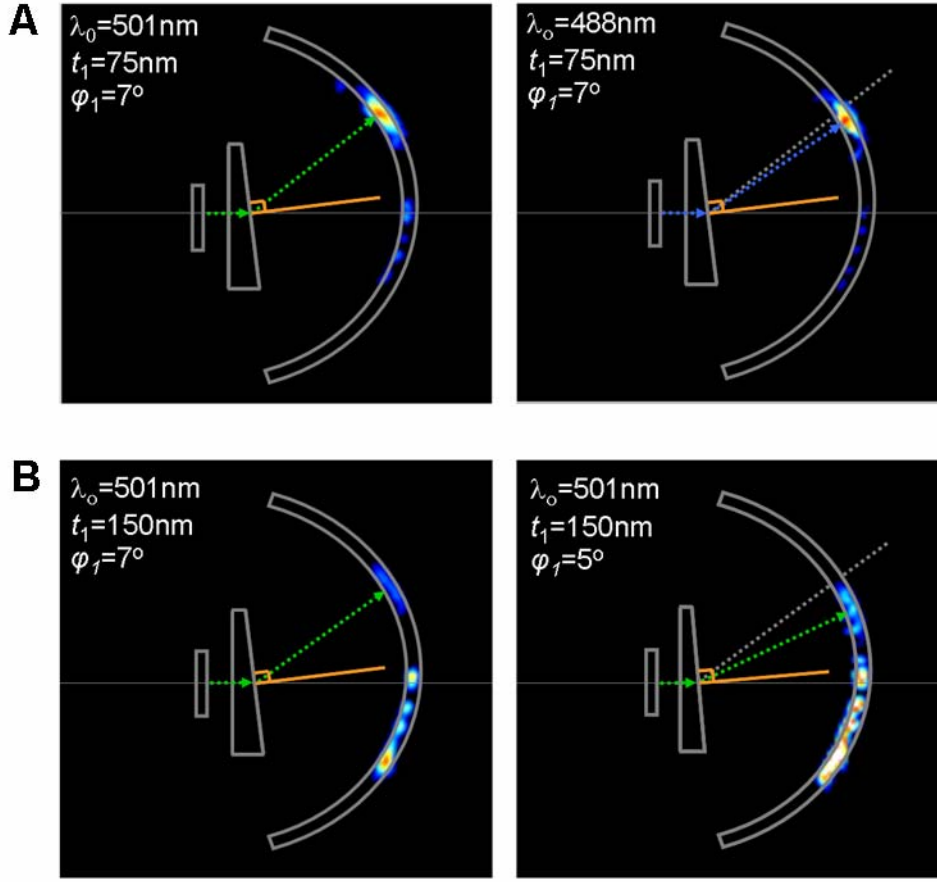
## 3. Effect of thickness and edge angle of Au/Si<sub>3</sub>N<sub>4</sub>/Ag prism

We characterize in detail the refractive properties of a Ag/Si<sub>3</sub>N<sub>4</sub>/Au waveguide within its frequency interval of negative refractive index. The result of refraction from a single prism of Ag/Si<sub>3</sub>N<sub>4</sub>/Au waveguide (W1), of dielectric-core thickness  $t_1 = 75 \text{ nm}$ , into a thick Ag/Si<sub>3</sub>N<sub>4</sub>/Ag waveguide (W2), of dielectric core thickness  $t_2 = 500 \text{ nm}$ , is shown in Fig. S2 A, at two closely-spaced wavelengths of  $\lambda_0 = 501 \text{ nm}$  and  $\lambda_0 = 488 \text{ nm}$ , respectively. Given an incident angle of  $\varphi_1 = 7^\circ$  at the W1/W2 interface, substantially different refraction angles  $\varphi_2 = -31.2^\circ$  and  $-27.1^\circ$  are obtained in each case. Applying Snell's law (Eq. S1) using these angles of refraction and measured values  $n_2 = 0.65$  and  $0.57$ , respectively (Fig. S1 B), we obtain effective refractive indices  $n_1 = -2.72$  and  $-2.09$ , respectively. Weak transmission of a positively-refracted spot can also be observed, hinting that 75-nm-thick constrictions can support a strongly attenuated positive-index photonic mode in addition to the negative-index SPP mode. As the waveguide thickness is increased to  $t_1 = 150 \text{ nm}$ , the positively refracted spot increases in intensity: photonic mode transmission competes with the SPP mode (Fig. S2 B). While the negatively-refracted spot size is slightly reduced with respect to the input slit length, the positively-refracted spot is enlarged. Such variations in spot size likely result from focusing or diffraction effects dependant on both the sign and the magnitude of  $n_1$ .

To confirm the applicability of Snell's law to the bimetallic waveguide structures, we vary the angle of incidence  $\varphi_1$  by fabricating W1 prisms ( $t_1 = 150 \text{ nm}$ ) with edge angles of  $\theta = 5^\circ$  and  $7^\circ$  respectively. Refraction results at  $\lambda_0 = 501 \text{ nm}$  are shown in Fig. S2 B. A distinct negatively-refracted spot is obtained in both cases, implying a



**Fig. S1.** Experimental determination of refractive index  $n_2$  of thick Ag/Si<sub>3</sub>N<sub>4</sub>/Ag waveguide. **(A)** Cross-sectional diagram of interferometer used to determine  $n_2$ . The structure is a modified version of the device of Fig 2B, in which the optically opaque metal cladding on both sides of the dielectric core is replaced with a 150-nm-thick layer of Ag. This semi-transparent cladding allows for interference, at the output-slit position, between the transmitted waveguide mode and the partially transmitted incident illumination. Periodic modulation of the light emerging from the output slit as a function of slit-slit distance  $d$  yields the effective mode index of the waveguide ( $S_2$ ). **(B)** Measured output-slit intensity as a function of  $d$  for wavelengths within the predicted negative index-region. Distance  $d$  is varied from 1 to 3  $\mu\text{m}$  in 25-nm increments. The waveguide index is given by  $n_2 = \lambda_0 / P$ , where  $P$  is the period of modulation. For free-space wavelengths  $\lambda_0 = 476, 488, 496, 501$ , and  $514$  nm, the resulting indices in the Ag/Si<sub>3</sub>N<sub>4</sub>/Ag waveguide are  $n_2 = 0.40, 0.57, 0.50, 0.65$ , and  $0.82$ , respectively.



**Fig. S2.** Detailed exploration of refractive properties of Au/Si<sub>3</sub>N<sub>4</sub>/Ag waveguide in the negative index region. **(A)** Output-spot position for the single prism geometry of Fig. 2C as a function of wavelength. The core thickness and interface angle of the prism are held constant at  $t = 75$  nm and  $\theta = \varphi_1 = 7^\circ$ , respectively. The angle of refraction  $\varphi_2$  varies from  $-31.2^\circ$  to  $-27.1^\circ$  as  $\lambda_0$  is decreased from 501 to 488 nm. **(B)** Output-spot position for prism angles of  $\theta = \varphi_1 = 7^\circ$  and  $5^\circ$ . Here, the core thickness and excitation wavelength are held constant at  $t = 150$  nm and  $\lambda_0 = 501$  nm, respectively. The angle of the negatively-refracted spot shifts from  $-28.8^\circ$  (for  $\varphi_1 = 7^\circ$ ) to  $-20.0^\circ$  (for  $\varphi_1 = 5^\circ$ ), corresponding to a constant prism index  $n_l = -2.5$  and confirming the applicability of Snell's Law to such waveguides operating in the negative index region. Note that in both **A** and **B**, bands of positive and negative refraction be observed, corresponding to transmission of a positive-index photonic mode and a negative-index plasmonic mode, respectively.

refraction angle of  $\varphi_2 = -20.0^\circ$  when  $\varphi_1 = 5^\circ$  and of  $\varphi_2 = -28.8^\circ$  when  $\varphi_1 = 7^\circ$ . The corresponding ratio  $\sin(\varphi_2)/\sin(\varphi_1) = n_1/n_2$  is  $-3.82$  and  $-3.88$ , respectively. The constancy of this ratio as a function of edge angle implies that Snell's law indeed applies to the present structures operating in the negative index region.

## References

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